



## **A scoping review on the use of machine learning in research on social determinants of health: Trends and research prospects**

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# Differentiation in corrosion performance of alumina forming alloys in alkali carbonate melts

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## ABSTRACT

Alkali carbonate melts are promising high temperature thermal storage media. In this work five alumina forming alloys have been exposed to a ternary LiNaK carbonate melt and CO<sub>2</sub> at 800 °C. The corrosion propagation was found to depend on the formation of a slow-growing LiAlO<sub>2</sub> scale. Furthermore, the two polymorphs contributing to the LiAlO<sub>2</sub> phase were monitored for up to 1000 h: a dense α-LiAlO<sub>2</sub> scale and γ-LiAlO<sub>2</sub> crystallites. We suggest a growth stress assisted formation of α-LiAlO<sub>2</sub> relaxing into the outwards growing γ-LiAlO<sub>2</sub> phase. This implies a deceleration of the α-LiAlO<sub>2</sub> scale growth towards a steady state-thickness.

## 1. Introduction

New generations of climate-neutral energy technologies, such as concentrated solar power (CSP) with thermal storage capacities, surpass current temperature limitations by utilising high temperature heat transport and storage media with superior thermal stability [1–5]. While reaching for increased energy conversion efficiency and grid stability, material challenges due to high temperature corrosion risks lack data on long-term performance, especially when it comes to selected molten salt mixtures in contact with metal components. These eutectic melts comprise commonly ternary alkali carbonates or binary chloride mixtures. The first pilot plant operating with ternary carbonates comprising lithium-, sodium, and potassium carbonates (LiNaK) operates at 700 °C [1].

Metal components are made of high temperature resistant alloys providing structural strength as well as containment of the salt, while growing a passivating oxide scale at the surface, preventing corrosion by molten species. Formation and slow growth of a passivating oxide scale are crucial for alloy components' overall performance and, subsequently, the entire power plant. Chromium oxide on stainless steels and aluminium oxide on ferritic alumina forming alloys are common candidates to establish a high temperature corrosion protection in next-generation thermal storages utilising alkali carbonates at 700 °C or higher. However, a chromium oxide scale has proven insufficient to protect an alloy against internal oxidation and rapid carburisation,

causing material embrittlement [6,7]. On the other hand, studies on alumina forming alloys showed that slow-growing alkali aluminate scales do not permeate carbon [8,9]. In this aspect, alumina forming alloys are superior to all chromia forming steels. In a previous study [7], we report specifically on the time-resolved performance of the alumina forming Kanthal® APMT at 800 °C immersed in LiNaK carbonates. Lithium ions have shown to be the predominant alkali species incorporated into oxides growing on high-temperature alloys [7,10,11]. After 72 h, the surface was covered by an α-lithium aluminate layer. After a few hundred hours, larger crystallites have been observed and identified as γ-lithium aluminate.

In the spirit of identifying the higher temperature operation limit, this research was conducted at 800 °C.

The solid-state synthesis of LiAlO<sub>2</sub> and characterisation of its two polymorphs α and γ has been published by Lehmann and Hasselbarth in 1961. In air, the low-temperature modification, α-LiAlO<sub>2</sub>, transforms into γ-LiAlO<sub>2</sub> at 600 °C or higher [12]. In several studies, reacting lithium carbonate with alumina powder in different environments revealed that the upper-temperature limit for α-LiAlO<sub>2</sub> formation is in the range of 747–777 °C [13–16].

Evans et al. introduced in 1978 a concept for the stress assisted formation of a duplex oxide scale comprising two polymorphs, i.e., tetragonal and monoclinic zirconia on zircaloy-2 [17]. In the present study, the same concept is adopted to express the growth of both α- and γ-LiAlO<sub>2</sub> at 800 °C. In Evans's case, a stress stabilised tetragonal zirconia

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morphology forms at the metal/oxide interface under compressive stress until relaxing into a monoclinic lattice. The magnitude of the compressive stress allows tetragonal  $\text{ZrO}_2$  to form at a significantly lower temperature than its ambient pressure phase transition point, as indicated in the T-P-phase diagram [18]. Detailed investigations are still regularly published to understand and predict a limiting scale thickness [19,20], also referred to as steady-state thickness, due to its technological importance for nuclear applications [19]. Evans et al. emphasised in 1978 that the concept of a stress stabilised inner oxide scale is universal under the condition of two possible polymorphs. We believe that the  $\alpha$ - to  $\gamma$ - $\text{LiAlO}_2$  transformation is one of these examples, which leads to the assumption of a limiting steady-state thickness of the  $\alpha$ - $\text{LiAlO}_2$  inner oxide layer.

It should be mentioned that the density of  $\gamma$ - $\text{LiAlO}_2$  is 25% lower compared to  $\alpha$ - $\text{LiAlO}_2$ . The crystal structure visualisation in Fig. 1 [21, 22] highlights the layered packing of lithium and aluminium ion polyhedrons along the c-axis for  $\alpha$ - $\text{LiAlO}_2$ , while  $\gamma$ - $\text{LiAlO}_2$  comprises alternating Li/Al tetrahedrons [22].

In this study, the corrosion processes on the alumina forming alloys Kanthal® APMT, Kanthal® AF, Nikrothal® PM58, and two newly developed alloys, Fe10Cr4Al base, in LiNaK carbonate melt at 800 °C will be described.

## 2. Experimental

Specimens of five alumina forming alloys have been prepared and investigated in this study. The alloys have relatively similar aluminium content. The nominal compositions of Kanthal® AF and Kanthal® APMT are almost identical, Fe20Cr5Al however, the latter differs in Mo and Mn content (Table 1.).

The newly developed Kanthal® EF100 and 101, Fe10Cr4Al, differ in Si content. Nikrothal® PM58 is an alumina-forming austenitic alloy.

A salt mixture of 32.1 wt%  $\text{Li}_2\text{CO}_3$ , 33.4 wt%  $\text{Na}_2\text{CO}_3$  and - 34.5 wt%  $\text{K}_2\text{CO}_3$  was prepared and have been purchased from VWR chemicals (99.0%), EMSURE anhydrous (99.9%), and ThermoFisher Scientific (99.8%), respectively.

The salt preparation method, chemical composition and concentration of each salt impurities are stated in [23]. A unique setup was built to provide a full immersion of coupons into the salt melt during exposures. A detailed description of the setup built is given in a previous publication [23]. The isothermal exposures were conducted at  $800 \pm 5$  °C under flowing  $\text{CO}_2$ . Upon each experiment, two duplicate samples are produced and are differently treated, as will be discussed further, depending on the characterisation technique. Each exposure was repeated at least two times for each material.

Metal coupons of initial measurements  $15 \times 15 \times 2$  mm were prepared to a mirror-like finish (1  $\mu\text{m}$  diamond polish). The polished samples were thoroughly cleaned and dried, then immersed in the prepared salt mixture. Detailed procedure of metal coupons preparation is provided in a former publication [23].

### 2.1. Post-exposure surface analysis

After exposure, samples were differently treated based on the type of investigations required. For example, samples subjected to surface investigations, X-ray diffraction (XRD) analysis, and mass change measurements have been rinsed with water by an ultrasonic cleaner at room temperature, see [23]. After weighing the washed samples, surface investigations were conducted by scanning electron microscopy (SEM) and energy-dispersive X-ray spectroscopy (EDX) using a JEOL JSM-7800F Prime or Phenom ProX Desktop SEM with an EDX detector. The Siemens D5000 powder diffractometer equipped with a Cu source, a secondary Si monochromator, and a point detector with grazing-incidence geometry was used for XRD surface analysis. Li containing species were exclusively detectable through XRD.

Rietveld refinement on the acquired XRD patterns was performed using the TOPAS V6 software. Rietveld refinement on the phases included zero-error corrections, polarisation factor, a fundamental parameters approach for instrumental profile simulation, preferred orientation correction based on spherical harmonics, corresponding emission profile, and polynomial simulated background. The structures used in the refinement were trigonal R-3 M for the  $\alpha$ - $\text{LiAlO}_2$  phase, tetragonal P41212 for the  $\gamma$ - $\text{LiAlO}_2$  phase, and cubic Im-3 m for the FeCrAl substrate phase.

It has to be noted that the applied model does not include absorption effects in the layered structure. Signal from the inner oxide layer will be decreased by the growing outer scale, affecting the measured peak intensities. In addition, the penetration depth in the used grazing incidence geometry cannot be determined without exact incidence angle values and densities (packing) of the probed layers. Hence, the obtained phase fractions provide only qualitative insights and require additional parameters obtained by microscopic inspection of cross-sections.

### 2.2. Post-exposure cross-section analysis

For cross-sectional investigations, samples were not rinsed. After pouring out the melt, a thin salt film stays on the top of the sample. Cross-sections of the exposed samples were prepared via dry cutting with a low-speed diamond saw, followed by broad ion beam (BIB) milling with a Leica TIC 3X instrument.

## 3. Results

In this section, the corrosion behaviour of the selected alumina forming alloys will be discussed based on mass change measurements, XRD and Rietveld analysis, and microscopic investigations (surface morphology and cross-sectional analysis).

### 3.1. Mass change measurements of alumina forming alloys exposed to alkali carbonate melts

Corrosion performance is evaluated quantitatively by measuring the

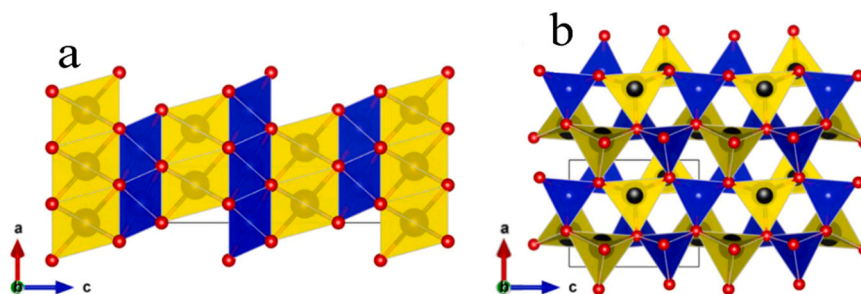


Fig. 1. Three-dimensional polyhedral visualisation of a)  $\alpha$ - $\text{LiAlO}_2$  and b)  $\gamma$ - $\text{LiAlO}_2$  crystal structures, where red, yellow and blue spheres represent oxygen, lithium and aluminium atoms [21,22].

**Table 1**  
Nominal alloy compositions.

Alloy	Fe	Ni	Cr	Al	Si	Mn	Mo	Others
Kanthal® APMT	balance	X	21	5	0.7	0.4	3	RE; C 0.08
Kanthal® AF	balance	X	21	5.3	0.7	X	X	RE; C 0.08
Kanthal® EF101	balance	< 0.5	11–14	3.2–4.2	1.2	< 0.7	X	RE; C 0.08
Kanthal® EF100	balance	< 0.5	9.5–13	3.8–4.2	< 0.5	< 0.7	X	RE; C 0.08
Nikrothal® PM58	18	Balance	19	5	0.4	X	X	RE

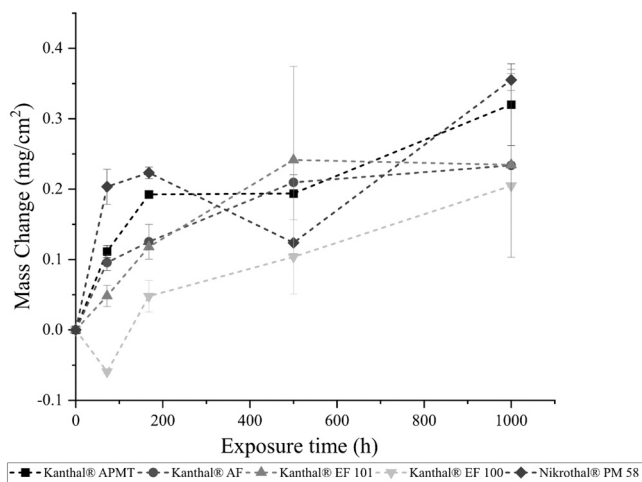
mass change of the samples after being rinsed with water [23]. Due to the rinsing procedure, the soluble oxide species are dissolved; therefore, the mass change values must be interpreted cautiously.  $\text{LiAlO}_2$  was not found to dissolve by this procedure. Nevertheless, the mass change plot, besides other analyses, can give an indication on the scale formation and growth kinetics. As shown in Fig. 2, all alumina forming alloys have shown relatively similar mass gain values. After 72 h, the mass gain obtained shows that Kanthal® EF 101 has the lowest mass gain, followed by Kanthal® APMT and Kanthal® AF, which have relatively similar mass change values; Nikrothal® PM58 has the highest mass gain, while the Kanthal® EF 100 has shown a mass loss.

The mass change data will be used in Table 2. to estimate  $\alpha/\gamma$ - $\text{LiAlO}_2$  phase transformation ratios, in comparison to the Rietveld data.

### 3.2. "Normal" formation and transformation of $\text{LiAlO}_2$

In this study, the selected alloys will be categorised into two groups based on their formation and transformation behaviour of  $\text{LiAlO}_2$ : i) "normal" and ii) "deviating". The "normal" formation and transformation of  $\text{LiAlO}_2$  is incorporating no ternary cationic species from the alloy and is therefore chemically very similar to the synthesis products already described by Lehmann and Hasselbarth [12]. The "deviating" behaviour described in the next chapter involves at least one more metal ion in the scale formation. Fig. 3. shows the XRD patterns of the Kanthal® EF 101 after exposure to alkali carbonate melts at 800 °C. After short-term exposure (72 h and 168 h), only one phase of  $\text{LiAlO}_2$  has been identified, i.e.  $\alpha$ - $\text{LiAlO}_2$ . After longer exposures (500 h and 1000 h), another lithium aluminate phase,  $\gamma$ - $\text{LiAlO}_2$  emerged. These findings are similar for Kanthal® APMT and Kanthal® AF. In Table 2. the  $\alpha/\gamma$   $\text{LiAlO}_2$  phase ratios are quantified by Rietveld analysis.

Fig. 4. displays the relatively similar surface morphology of Kanthal® APMT, Kanthal® AF, and Kanthal® EF 101. After short-term exposure (72/168 h), small crystals, identified as  $\alpha$ - $\text{LiAlO}_2$ , completely covered the surface. After longer exposure times (500 h/1000 h), the larger  $\gamma$ - $\text{LiAlO}_2$  phase started to emerge.



**Fig. 2.** Overall mass change behaviour of the selected alumina forming alloys immersed in alkali carbonate at 800 °C after different exposure times.

Fig. 5 shows an example of the characteristic double-layer structure composed of a compact inner  $\alpha$ - $\text{LiAlO}_2$  scale and outer  $\gamma$ - $\text{LiAlO}_2$  crystals, on Kanthal® EF 101. The average scale thicknesses of the "normal" behaving  $\text{LiAlO}_2$  forming alloys have been measured and tabulated in Table 2. Kanthal® APMT shows the thickest  $\alpha$ - $\text{LiAlO}_2$  scale among the "normal" behaving alloys.

The measured mass gain,  $\Delta m_{\text{(measured)}}$ , for the "normal"  $\text{LiAlO}_2$  formers represents the uptake of lithium and oxygen into the scale. The amount of substance ( $n$ ) for  $\text{LiAlO}_2$  is obtained by correcting the measured mass gain for the aluminium contribution from the alloy (41% of the molar mass  $M_{\text{LiAlO}_2}$ ) divided by the total  $M_{\text{LiAlO}_2}$ , Eq. 1. The  $\alpha$ - $\text{LiAlO}_2$  phase in the "normal" scenario forms a rather homogeneous scale at the surface with a mean thickness  $X(\alpha)$ . The mean thickness  $X(\alpha)$  derived from cross-sectional analyses multiplied by sample area and theoretical density of  $\alpha$ - $\text{LiAlO}_2$  from the crystallographic database [22] allows us to determine an approximate total mass of  $\alpha$ - $\text{LiAlO}_2$  and consequently an amount of substance,  $n(\alpha)$ .

$$n(\text{LiAlO}_2 \text{ total}) = n(\alpha) + n(\gamma) = \frac{\Delta m_{\text{(measured)}} \cdot 1.69}{M(\text{LiAlO}_2)} \quad (1)$$

For each sample of the "normal"  $\text{LiAlO}_2$  formers, the  $\alpha/\gamma$ -phase ratio was determined using Eq. 1, combining gravimetry and microscopy. Rietveld refinement for each powder diffractogram has been used as an alternative quantification of  $\alpha/\gamma$ - $\text{LiAlO}_2$  ratios for comparison.

The  $\alpha/\gamma$  phase ratios derived by Rietveld refinement contain information on the increasing coverage of the sample surfaces by  $\gamma$ - $\text{LiAlO}_2$ . The ratios determined by combined microscopy and gravimetric measurements allow for a quantification of the  $\alpha$ - $\text{LiAlO}_2$  scale contribution to the total mass gain. All values are tabulated in Table 2. It is noteworthy that the mass gain and scale thickness used in the calculations are for two different coupons. However, they have been exposed simultaneously under the same conditions.

Plotting scale thicknesses and the  $\alpha/\gamma$ -phase ratio (Rietveld) in Fig. 6. reveals the growth of  $\alpha$ - and  $\gamma$ - $\text{LiAlO}_2$  phase over time. It is noteworthy to point out that the  $\alpha/\gamma$  ratios derived by Rietveld analysis plotted in Fig. 6 seem to indicate a deceleration or even reducing  $\gamma$ - $\text{LiAlO}_2$  fraction after 500 h for Kanthal APMT and Kanthal EF101, while the average thickness is steadily increasing. The top view images in Fig. 4. show that the individual  $\gamma$ - $\text{LiAlO}_2$  crystals grow significantly with time but the overall number of nucleation sites does not increase. This can have an effect on the Rietveld phase fraction slope in Fig. 6. The rapid increase of size and phase fraction of  $\gamma$ - $\text{LiAlO}_2$  may lead to Al depletion in the bulk alloy. Thus, line scan analysis has been performed on all 1000 h exposure samples and did not substantiate that concern (Fig. 5.d). The  $\alpha$ - $\text{LiAlO}_2$  scale growth decelerates over time.

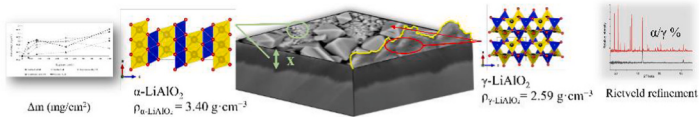
Summarising the observations for the "normally" behaving  $\text{LiAlO}_2$  forming alloys, minor deviations can be found for each parameter, i.e., as surface roughness, crystals size and scale thickness.

### 3.3. "Deviating" formation and transformation of $\text{LiAlO}_2$

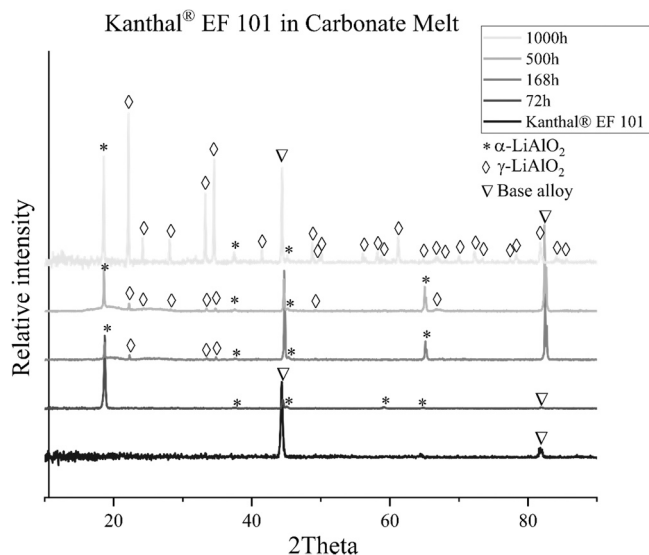
The corrosion behaviour of the Kanthal® EF 100 and Nikrothal® PM 58 deviates from the "normal"  $\alpha$ - $\text{LiAlO}_2$  forming alloys, particularly after short-term exposures. In the case of Kanthal® EF 100, the alloy surface was completely covered with  $\text{LiFeO}_2$  crystals after 72 h, as shown in Fig. 7.c and confirmed with XRD, Fig. 8. After 168 h, however, all traces

**Table 2**

Mean scale thicknesses (X) for  $\alpha$ - and  $\gamma$ -LiAlO<sub>2</sub>, mass change  $\Delta m$ , gravimetrically and microscopically derived  $\alpha/\gamma$ -phase ratio (calc. Eq. 1) and Rietveld derived phase ratios ( $\alpha$  to  $\gamma$  % Rietveld). The n.a. (not available) error data in the table is attributable to duplicate sample loss in the repeated experiment due to alumina crucible breakdown during cooling.



Exposure Time	$\Delta m$ (mg/cm <sup>2</sup> )	X <sub>measured</sub> ( $\mu m$ )	$\alpha$ to $\gamma$ % calc.	$\alpha$ to $\gamma$ % Rietveld
<b>Kanthal<sup>®</sup> APMT</b>				
72 h	$\alpha$	0.11±0.008	0.30 (Max 0.6)	97.33
	$\gamma$		-	2.67
168 h	$\alpha$	0.19±n.a.	0.75 (Max 2.4)	77.05
	$\gamma$		-	22.95
500 h	$\alpha$	0.19±0.002	0.95 (Max 3.2)	63.9 ± 0.9
	$\gamma$		1.60 (Max 2.3)	36.1 ± 0.9
1000 h	$\alpha$	0.32±0.06	1.80 (Max 3.2)	78.1 ± 1.1
	$\gamma$		5.2 (Max 8.8)	21.9 ± 1.1
<b>Kanthal<sup>®</sup> AF</b>				
72 h	$\alpha$	0.10±0.01	0.45 (Max 0.7)	93.79
	$\gamma$		-	6.21
168 h	$\alpha$	0.13±0.02	0.5 (Max 0.7)	85.5±2.5
	$\gamma$		0.42 (Max 0.6)	14.5±1.9
500 h	$\alpha$	0.21±0.01	0.6 (Max 0.7)	70±1
	$\gamma$		0.85 (Max 4.4)	30±1
1000 h	$\alpha$	0.23±0.13	1.13 (Max 1.8)	9.8±2.5
	$\gamma$		3.0 (Max 4.3)	90.2±2.4
<b>Kanthal<sup>®</sup> EF 101</b>				
72 h	$\alpha$	0.05±0.01	0.45 (Max 1.2)	100
	$\gamma$		-	0
168 h	$\alpha$	0.12±n.a.	0.47 (Max 0.6)	64±0.9
	$\gamma$		0.75 (Max 1.25)	36±0.9
500 h	$\alpha$	0.24±0.13	0.52 (Max 0.7)	18±5
	$\gamma$		1.4 (Max 2.7)	82±5
1000 h	$\alpha$	0.23±n.a.	0.6 (Max 1.1)	20.2±3.8
	$\gamma$		1.7 (Max 3.5)	79.8±3.3



**Fig. 3.** XRD patterns of Kanthal<sup>®</sup> EF 101 after exposure to alkali carbonates in CO<sub>2</sub> at 800 °C for 72 h, 168 h, 500 h and 1000 h.

of LiFeO<sub>2</sub> have disappeared due to dissolution into the carbonate melt (Fig. 7d and g). This observation is in agreement with the observed mass loss, cf. Fig. 2. Instead, small crystals of  $\alpha$ -LiAlO<sub>2</sub> are formed. Furthermore, after longer exposure times (500 h/1000 h),  $\gamma$ -LiAlO<sub>2</sub> crystals started to grow similarly to the "normally" behaving alloys. Due to the initial mass loss induced by the transient  $\alpha$ -LiFeO<sub>2</sub>, the coupled gravimetric/microscopic determination of the  $\alpha/\gamma$ -LiAlO<sub>2</sub> phase ratio via Eq. 1 was not applicable here. However,  $\alpha/\gamma$ -LiAlO<sub>2</sub> phase ratios have been obtained by Rietveld refinement of the XRD patterns obtained after 168 h, 500 h and 1000 h exposures. The Rietveld data and mean scale thicknesses are shown for comparison in Fig. 6. Indeed, the slow growth of the thin  $\alpha$ -LiAlO<sub>2</sub> scale and scarce nucleation of  $\gamma$ -LiAlO<sub>2</sub> crystallites at the surface lead us to classify Kanthal<sup>®</sup> EF 100 as one of the "normally" behaving LiAlO<sub>2</sub> forming alloys after overcoming a deviating early stage.

At 800 °C the austenitic alloy Nikrothal<sup>®</sup> PM58 forms Li(Cr,Al)O<sub>2</sub> in contrast to the protective  $\alpha$ -LiAlO<sub>2</sub> scale that has been reported for exposures at 750 °C [24]. Fig. 9. shows XRD and microscopic analysis results of Nikrothal<sup>®</sup> PM58 after exposure to alkali carbonate melts for at least 1000 h. Cross-section and EDX analyses revealed that Nikrothal<sup>®</sup> PM58 developed pegs in the suboxide zone filled with mainly Li(Cr,Al)O<sub>2</sub> and some fractions of aluminium enriched scale as well as nickel and iron-rich particles. In Fig. 9.c–e, point analysis on the surface reveal that Fe and Ni particles have been transported to the oxide/melt interface

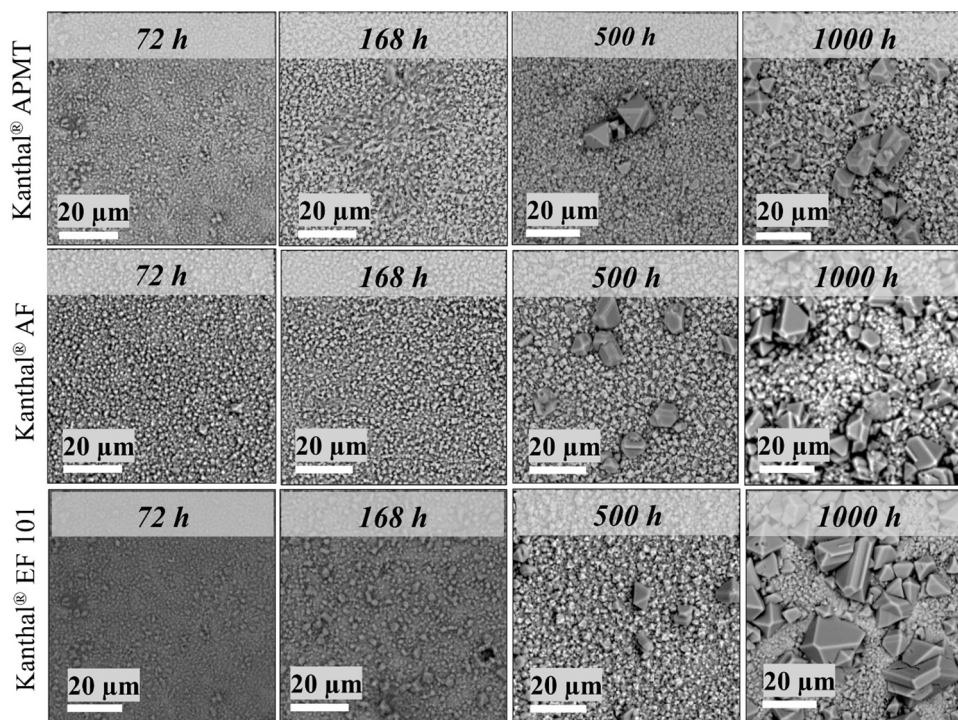


Fig. 4. Top view electron microscopic images for "normal behaving alloys" only LiAlO<sub>2</sub> species exposed to carbonate melts at 800 °C after different exposure times. Larger crystals present γ- LiAlO<sub>2</sub>, small crystals are attributed to α- LiAlO<sub>2</sub>.

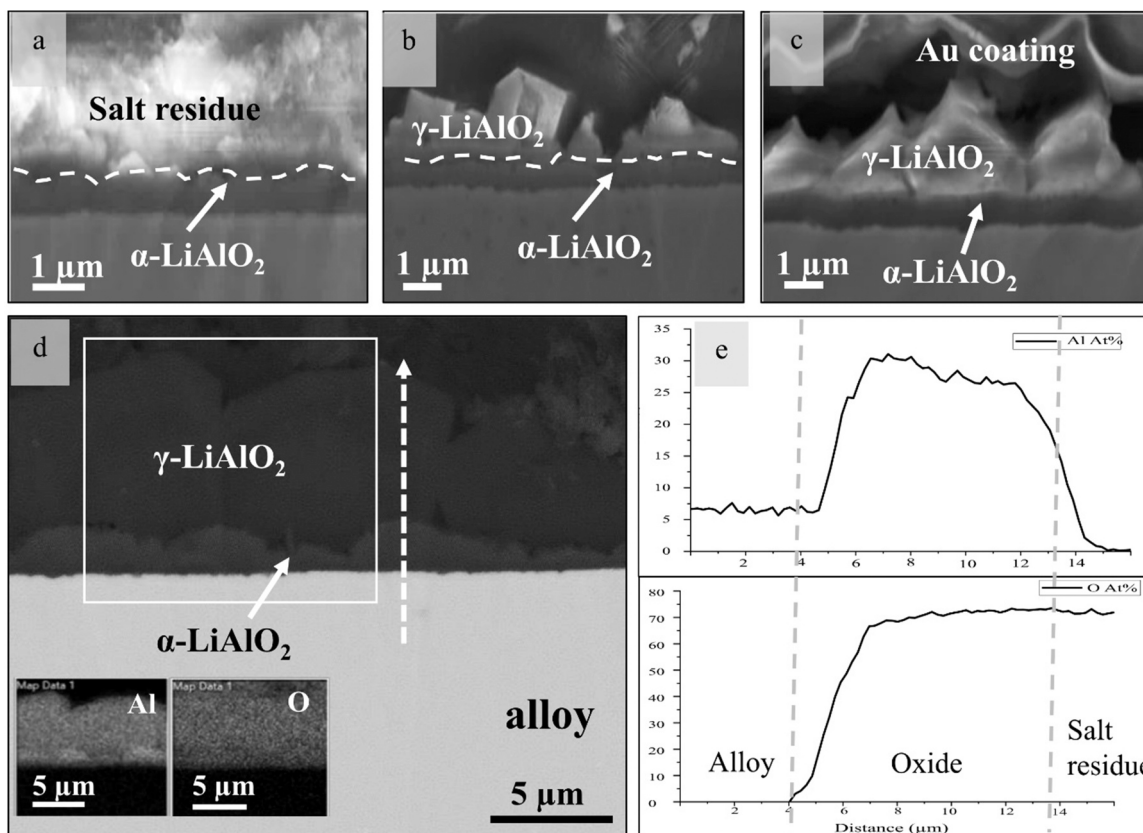


Fig. 5. Cross-section of Kanthal® EF 101 immersed in LiNaK carbonate at 800 °C after a) 72 h, b) 168 h, c) 500 h and d) 1000 h and EDS mapping of Al and oxygen through crystals, e) line scans of Al and oxygen through crystals and in the bulk alloy.

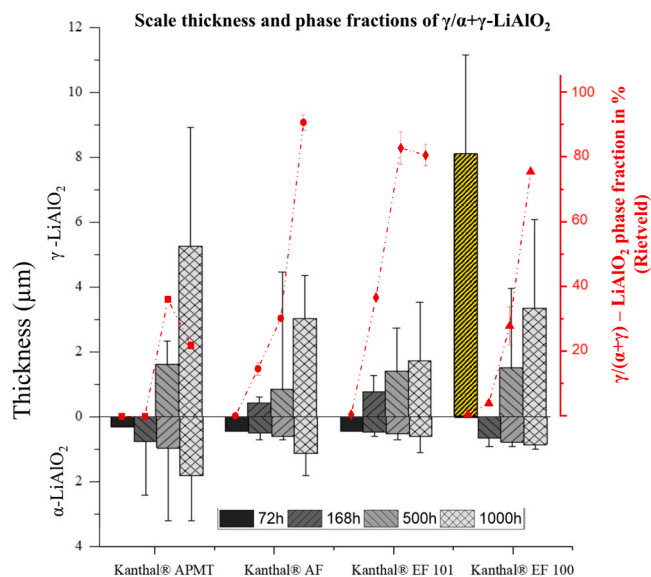


Fig. 6. Thickness values for  $\alpha$ - and  $\gamma$ -LiAlO<sub>2</sub> of the four ferritic FeCrAl alloys and the corresponding results of Rietveld analysis, Column in yellow represents LiFeO<sub>2</sub> cf. Section 3.3.

and can easily leach into the alkali carbonate melt. An aluminium depletion zone in the suboxide region has been detected, reaching roughly 14 μm into the alloy. Just beneath the oxide, the aluminium content was lowered by 1.2 wt% compared to the nominal composition (see Fig. 9.f).

#### 4. Discussion

From the experimental results, two fundamental oxidation behaviours of alumina formers in alkali carbonate melts can be distinguished. One we call the "normal" lithium aluminate formation with an initially forming inner  $\alpha$ -LiAlO<sub>2</sub> and an outer  $\gamma$ -LiAlO<sub>2</sub> phase. No other cationic

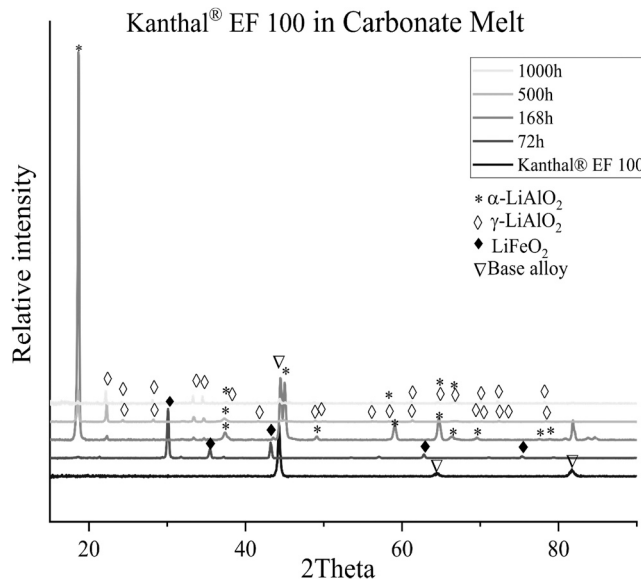


Fig. 8. XRD patterns for Kanthal® EF 100 after exposure to alkali carbonates in CO<sub>2</sub> at 800 °C for 72 h, 168 h, 500 h and 1000 h.

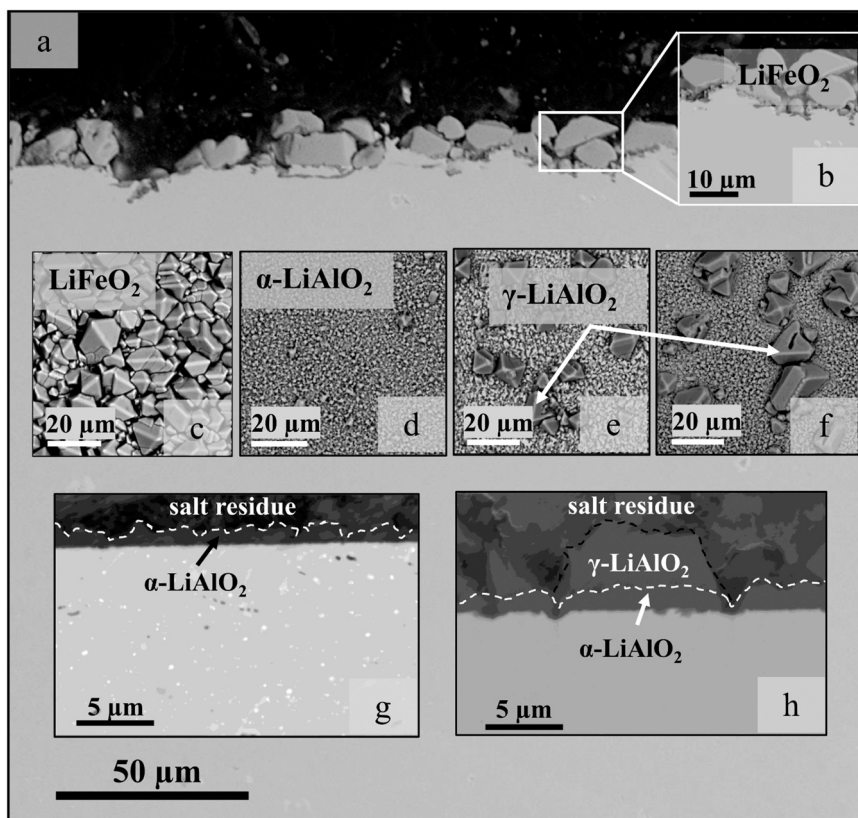
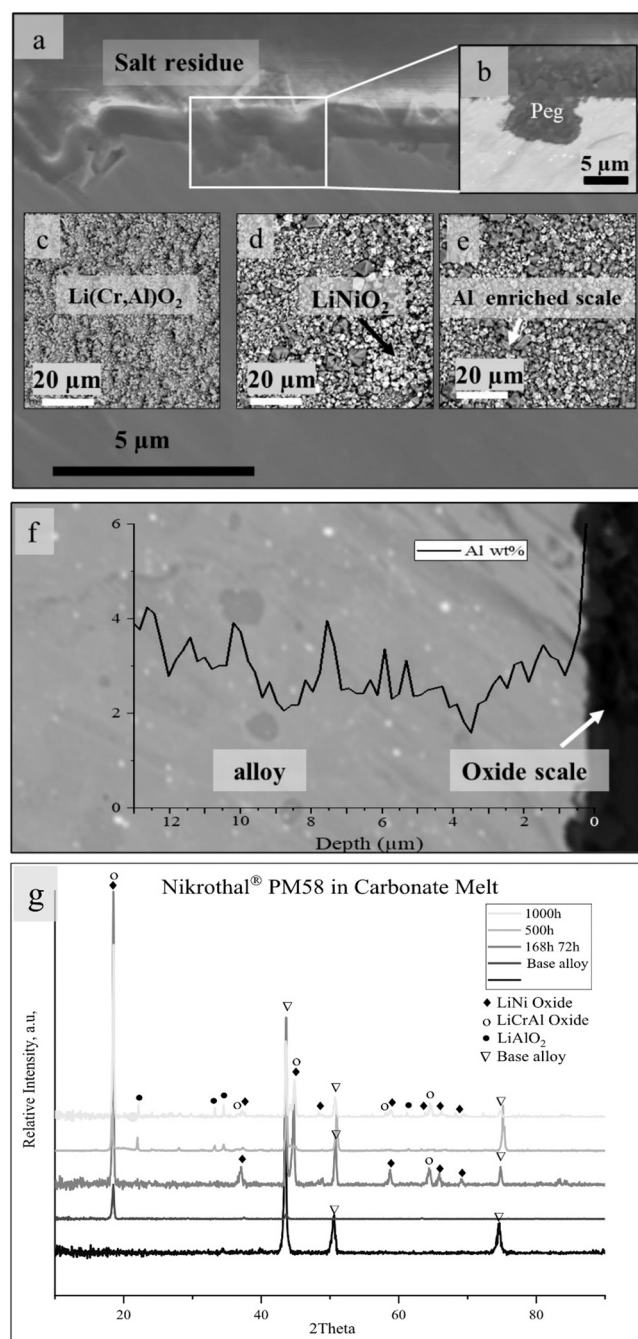


Fig. 7. Top view of Kanthal® EF 100 exposed to alkali carbonate melts at 800 °C, a, b) Cross section after 72 h. Top-view image of c) 72 h, LiFeO<sub>2</sub> covers the surface, d) 168 h, only  $\alpha$ -LiAlO<sub>2</sub> covers the surface, e) 500 h,  $\gamma$ -LiAlO<sub>2</sub> crystallites appear, f) 1000 h,  $\gamma$ -LiAlO<sub>2</sub> crystallites size increased. Cross-section after g) 168 h, h) 1000 h.



**Fig. 9.** Nikrothal® PM58 exposed to alkali carbonate melts at 800 °C, Cross-section after a) 1000 h in SEM contrast, b) peg after 1000 h in backscatter contrast. Top-view image after c) 72 h, Li(Cr,Al)O<sub>2</sub> covers the surface, d) 500 h, presence of nickel and iron-rich particles, e) 1000 h, Al enriched scale fractions, f) line scan for the suboxide zone after 1000 h, g) XRD patterns for Nikrothal® PM58 after exposure to alkali carbonates in CO<sub>2</sub> at 800 °C for 72 h, 168 h, 500 h and 1000 h.

species is interfering or detected on the scale. Every other behaviour has been denominated "deviating" oxidation of alumina forming alloys in contact with alkali carbonates involving transient oxide formation and pegging.

#### 4.1. "Normal" LiAlO<sub>2</sub> formation and transformation

"Normal" LiAlO<sub>2</sub> formation was observed for the alloys Kanthal® AF, Kanthal® APMT and Kanthal® EF 101. Exposure experiments in alkali

carbonates at 800 °C revealed formation of a covering α-LiAlO<sub>2</sub> scale after 72 h. This homogeneous α-LiAlO<sub>2</sub> scale protects the bulk alloy against internal oxidation and carburisation.

Worth noting, α-LiAlO<sub>2</sub> is thermodynamically not favoured at 800 °C [13]; hence it is important to offer an understanding why the α-LiAlO<sub>2</sub> scale is present at this temperature and grows with time. At this point, we want to remind the reader of Evans' et al. oxidation mechanism for phase stabilisation under compressive growths stress [17]. α-LiAlO<sub>2</sub> has a significantly higher theoretical density compared to the γ-modification. Therefore, the growing α-LiAlO<sub>2</sub> scale is able to accommodate not only a higher amount of oxygen but also lithium ions in the same volume compared to γ-LiAlO<sub>2</sub> and thereby absorbing growth stresses. From a corrosion control point of view, α-LiAlO<sub>2</sub> is the preferential crystal morphology because it forms a dense scale that maintains a slow and gradual oxidation process.

However, in this study, we found the γ-LiAlO<sub>2</sub> morphology signal after 168 h in the XRD patterns for all ferritic alumina forming alloys in conjunction with larger faceted crystallites at the surface. γ-LiAlO<sub>2</sub> crystallites are free-standing at the melt/oxide interphase and do not experience compressive growth stresses.

The amount of both LiAlO<sub>2</sub> modifications increases with time, whereby α-LiAlO<sub>2</sub> is the only phase initially, while γ-LiAlO<sub>2</sub> takes quickly over, as shown in Fig. 6. Since the formation and growth of α-LiAlO<sub>2</sub> depends on the presence of compressive stresses, we, therefore, expect to find a steady-state behaviour of the inner scale. The stress relaxation will define the limiting inner α-scale thickness at the gas/oxide interface into the thermodynamically stable γ-modification. In this study, we have not reached the limiting α-scale thickness yet; however, its scale growth rate already significantly declines after 1000 h, while the γ-crystallites keep growing. Rietveld refinement also confirmed an increasing surface coverage of γ-LiAlO<sub>2</sub> with time.

The α-LiAlO<sub>2</sub> steady-state thickness is expected to be temperature-dependent. At temperatures below 750 °C, α-LiAlO<sub>2</sub> is the thermodynamically dominating morphology and therefore, γ-LiAlO<sub>2</sub> nucleation is unexpected.

Due to the fast growth and individual crystallinity, γ-LiAlO<sub>2</sub> limits the lifetime of the alloy in the melt in two ways. On the one hand, the absence of the covering α-LiAlO<sub>2</sub> scale and consequently poor diffusion barrier increases accessibility of corrosion species to the metal surface. On the other hand, the faster growth of γ-LiAlO<sub>2</sub> crystallites accelerates the depletion of aluminium from the alloy eventually compromising the formation of a protective α-LiAlO<sub>2</sub> scale.

#### 4.2. "Deviating" LiAlO<sub>2</sub> formation and transformation

Two of the alumina forming alloys, Kanthal® EF 100 and Nikrothal® PM58, investigated in this study, have not shown the here called "normal" LiAlO<sub>2</sub> scale evolution.

As shown in the results for 800 °C, Kanthal® EF 100 presents with an external lithium ferrite, LiFeO<sub>2</sub>, after 72 h. After 168 h, the LiFeO<sub>2</sub> phase has disappeared, presumably due to dissolution, and a "normal" LiAlO<sub>2</sub> scale has formed and remained at least until the end of the experiment. Lacking the beneficial silicon content, Kanthal® EF 100 rapidly grows initially a covering LiFeO<sub>2</sub> scale. After reaching a sufficiently high thickness (~8.0 μm after 72 h), oxygen and lithium activities are low enough to nucleate a slow-growing LiAlO<sub>2</sub> at the metal/scale interface, decreasing the growth significantly. LiFeO<sub>2</sub> is leachable into the melt and has dissolved completely after 168 h. This LiAlO<sub>2</sub> undergoes further α- to γ- transformation as described in the former section on "normal" LiAlO<sub>2</sub> formation.

This result is very similar to observations made by comparing the oxidation behaviour of Kanthal® EF 100 and Kanthal® EF 101 in dry air [25].

Even though the chemical composition for both alloys is very similar, differing exclusively in silicon content, Kanthal® EF 101 grows reliably on an aluminium oxide scale in the referenced case in dry air while

Kanthal® EF 100 rapidly grows iron oxide instead [25].

Of note, the newly developed Kanthal® EF 100 and Kanthal® EF 101 have been used in former publications under names “model alloy 198” and “model alloy 197”, respectively.

The silicon contribution to the protective alumina scale formation is addressed as 3rd element effect. In our study here, the 3rd element effect of silicon as alloying element extends even beneficially for the reliable formation of  $\alpha$ -LiAlO<sub>2</sub> in carbonate melts.

Nikrothal® PM58 deviates in another way from all other exposed alumina forming alloys investigated in this study. As austenitic alumina forming alloy, aluminium diffusion towards the metal/scale interface is a priori slower than for the four ferritic alloys [26], as seen in the flat aluminium profile in the suboxide region (Fig. 9.f). As described in Section 4.1. on “normal” LiAlO<sub>2</sub> formation, an intact  $\alpha$ -LiAlO<sub>2</sub> can only be maintained by a steady-state supply of aluminium to the metal/scale interface. A covering  $\alpha$ -LiAlO<sub>2</sub> scale could not be detected after exposure to alkali carbonates at 800 °C. This result strongly contrasts with an earlier study also undertaken in the same lab revealing that a protective slow-growing scale was formed and sustained at 750 °C for at least 740 h [24]. This observation indicates a strong correlation with the temperature dependence of LiAlO<sub>2</sub> phase transition investigated by [13], where the lower limit for  $\gamma$ -LiAlO<sub>2</sub> formation was indeed 750 °C.

## 5. Conclusions

All ferritic alumina forming alloys investigated in this study formed a dense and adherent  $\alpha$ -LiAlO<sub>2</sub> scale after max. 168 h at 800 °C, fully immersed in alkali carbonates under flowing CO<sub>2</sub>. This scale grows slowly and protects the alloy from internal oxidation and carburisation, which are common major corrosion problems for chromia forming high temperature alloys in contact with carbonates or CO<sub>2</sub>.

However, the  $\alpha$ -LiAlO<sub>2</sub> forms initially due to growth stress. On top of the  $\alpha$ -LiAlO<sub>2</sub> scale, the thermodynamically stable  $\gamma$ -LiAlO<sub>2</sub> nucleates and rapidly grows non-protective crystals. Up to 1000 h of exposure, no detrimental aluminium depletion from the alloys was reached. The austenitic alloy Nikrothal® PM58 does not grow the preferable  $\alpha$ -LiAlO<sub>2</sub> at 800 °C due to the relatively slow diffusion of aluminium from the alloy towards the alloy/melt interface.

## CRedit authorship contribution statement

**Esraa Hamdy:** Conducting exposure experiments, sample analyses, main author of this article. **Michal Strach:** Using Rietveld refinement method, TOPAS V6 software,  $\alpha/\gamma$ -LiAlO<sub>2</sub> phase fraction calculations, co-authoring this article. **Johanna Nockert Olovsjö:** Sample material advisor and main project partner for materials supplying at Kanthal, co-authoring this article. **Christine Geers:** Conducting exposure experiments, sample analyses, co-authoring this article.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Data Availability

The raw/processed data required to reproduce these findings will be made available upon request. Additional data of a previous publication can be found [23].

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